ME 115(b): Solution to Problem Set #4

Problem #1: Problem 2(b,d) of Chapter 5 in MLS text. Part (b.)

Yes, this grasp is force closure.

Part (d.) $B_1, B_2 = I.$

$$G_{1} = \begin{bmatrix} I & S \begin{bmatrix} 0 \\ -a \\ b \end{bmatrix} \\ 0 & I \end{bmatrix} B_{1}$$
$$G_{2} = \begin{bmatrix} I & S \begin{bmatrix} 0 \\ a \\ b \end{bmatrix} \\ 0 & I \end{bmatrix} B_{1}$$

The complete grasp matrix is

$$G = \begin{bmatrix} G_1 & G_2 \end{bmatrix}$$

Note that each G_i is full rank (since $B_i = I$).

Force-closure \longleftrightarrow G is full rank and there exists $F_N \in \eta(G)$ such that $F_N \in FC$. But G is full rank since each G_i is full rank. Furthermore, it has a null space of dimension 6 (nullity + rank =12) and since FC = $\Re^6 \times \Re^6$, every $F_N \in \eta(G)$ is in FC. Therefore, force closure $\dim(\eta(\mathbf{G})) = 12 - rankG = 6.$

The grasp is *not* manipulable. The grasping constraint is

$$\begin{bmatrix} B_1^T & T_{C_1S} & J_1 & 0\\ 0 & B_2^T & T_{C_2S} & J_2 \end{bmatrix} \dot{\theta} = G^T \begin{pmatrix} V_0\\ \omega_0 \end{pmatrix} = \begin{bmatrix} G_1^T\\ G_2^T \end{bmatrix} \begin{pmatrix} V_0\\ \omega_0 \end{pmatrix}$$

Since G_1^T is full rank, we must have $\Re(B_1^T T_{C_1S} J_1) \supseteq \Re(G_1^T) = \Re^6$. But $J_1 \in Re^{6 \times 4} \longrightarrow$ its range has dimension 4 away from singularities, therefore the grasp is not manipulable.

Problem #2: Problem 3(b) of Chapter 5 in MLS text.

$$R_{C_1} - \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{bmatrix}$$

$$\hat{P}_{C_1} = \begin{bmatrix} 0 \\ -r \\ 0 \end{bmatrix}$$
$$\hat{P}_{C_1} = \begin{bmatrix} 0 & 0 & -r \\ 0 & 0 & 0 \\ r & 0 & 0 \end{bmatrix}$$
$$R_{C_2} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix}$$
$$\hat{P}_{C_2} = \begin{bmatrix} 0 \\ r \\ 0 \end{bmatrix}$$
$$\hat{P}_{C_2} = \begin{bmatrix} 0 \\ r \\ 0 \end{bmatrix}$$

Plugging these into equations for G_i :

Plugging $G_i {\rm s}$ into the overall Grasp Map gives:

$$G = \begin{bmatrix} G_1 & G_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & -1 & 0 \\ 1 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ -r & 0 & 0 & 0 & 0 & r & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & -1 \\ 0 & r & 0 & 0 & -r & 0 & 0 & 0 \end{bmatrix}$$

Now to write the friction cone conditions:

$$FC = FC_{C_1} \times FC_{C_2} \tag{1}$$

$$FC_{C_1} = \{ f_c : \sqrt{(f_{C_1}')^2 + (f_{C_1})^2} \le \mu f^3_{C_1}, \| f^4_{C_1} \| \le \gamma f^3_{C_1}, f^3_{C_1} \ge 0 \}$$
(2)

$$FC_{C_2} = \{ f_c : \sqrt{(f_{C_2}')^2 + (f_{C_2})^2} \le \mu f^3_{C_2}, \| f^4_{C_2} \| \le \gamma f^3_{C_2}, f^3_{C_2} \ge 0 \}$$
(3)

The grasp map is full rank. Additionally, the 'force closure by inspection' method shown in class shows that this is a force closure grasp since it is a soft-finger grasp and a line between the two contact points can be drawn which is fully enclosed by both friction cones.

Problem #3: Problem 4(a) of Chapter 5 in MLS text.

We can derive the wrench basis by looking at which directions are free to movement. This contact model does not allow movement in the x,y, and z directions, or rotation along the x or z axis. It does, however, allow rotation along the y axis.

Thus the wrench basis is:

[1	0	0	0	0
0	1	0	0	0
0	0	1	0	0
0	0	0	1	0
0	0	0	0	0
0	0	0	0	1

Friction cone:

$$\mu > 0 \tag{4}$$

$$\sqrt{f_x + f_y} \le \mu \cdot f_n \tag{5}$$

$$f_n \ge 0 \tag{6}$$

$$|\tau_n| \le \gamma_n f_n \tag{7}$$

$$|\tau_y| \le \gamma_y f_y \tag{8}$$

Problem #4: Problem 5(a) of Chapter 5 in MLS text.

There are many possible answers to this problem. The easiest is to choose an equilateral triangle. You can then show geometrically that there is no way that a line between two point contacts can be made such that it will pass through both friction cones (in the case where $\mu = \tan 30$.

Problem #5: Problem 8(b) of Chapter 5 in MLS text.

We have an equilateral triangle and we wish to find all possible force-closure grasps for two contacts with friction and a coefficient of friction, μ =tan 45. The constraints that the line between contacts lie in the relevant friction cones become:

$$A: (\eta_1 - \mu {\eta_1}^{\perp}) \otimes (p_2 - p_1) > 0$$
(9)

$$B: (\eta_1 + \mu \eta_1^{\perp}) \otimes (p_2 - p_1) < 0$$
(10)

$$C: (\eta_2 - \mu \eta_2^{\perp}) \otimes (p_1 - p_2) > 0$$
(11)

$$D: (\eta_2 + \mu \eta_2^{\perp}) \otimes (p_2 - p_1) < 0$$
(12)

$$\eta_1 = \begin{bmatrix} 0\\1 \end{bmatrix} \tag{13}$$

$$\eta_1^{\perp} = \begin{bmatrix} -1\\ 0 \end{bmatrix} \tag{14}$$

$$\eta_2 = \begin{bmatrix} \cos 30\\ -\sin 30 \end{bmatrix} = \begin{bmatrix} \frac{\sqrt{3}}{2}\\ -\frac{1}{2} \end{bmatrix}$$
(15)

$$\eta_2^{\perp} = \begin{bmatrix} \sin 30\\ \cos 30 \end{bmatrix} = \begin{bmatrix} \frac{1}{2}\\ \frac{\sqrt{3}}{2} \end{bmatrix}$$
(16)

$$p_1 = \begin{bmatrix} d_1 \\ 0 \end{bmatrix} \tag{17}$$

$$p_2 = \begin{bmatrix} d_2 \sin 30\\ d_2 \cos 30 \end{bmatrix} = \begin{bmatrix} \frac{1}{2}d_2\\ \frac{\sqrt{3}}{2}d_2 \end{bmatrix}$$
(18)

$$\mu = \tan 45 = 1 \tag{19}$$

Plugging in these values into A,B,C and D:

$$A: d_1 + d_2 \frac{\sqrt{3} - 1}{2} > 0 \tag{20}$$

$$B: d_1 - d_2 \frac{\sqrt{3} - 1}{2} < 0 \tag{21}$$

$$C: -\left(\frac{\sqrt{3}}{2} - \frac{1}{2}\right)\frac{\sqrt{3}}{2}d_2 + \left(d_1 - \frac{d_2}{2}\right)\left(\frac{1}{2} - \frac{\sqrt{3}}{2}\right) > 0$$
(22)

$$D: -\left(\frac{\sqrt{3}}{2} + \frac{1}{2}\right)\frac{\sqrt{3}}{2}d_2 - \left(d_1 - \frac{d_2}{2}\right)\left(\frac{\sqrt{3}}{2} + \frac{1}{2}\right) < 0$$
(23)

Problem #6:

Part #1: Yes, this grasp is force closure. We can use the visual method we learned last week, we can see that a line connecting the two point contacts clearly runs through both friction cones. **Part** #2:

$$R_{1} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{bmatrix}$$

$$P_{1} = \begin{bmatrix} 0 \\ -d \\ 0 \end{bmatrix}$$

$$R_{1} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix}$$

$$P_{1} = \begin{bmatrix} 0 \\ d \\ 0 \end{bmatrix}$$

$$WrenchBasis = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$G_{1} = \begin{bmatrix} R_{1} & 0 \\ \hat{P}_{1}R_{1} & R_{1} \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \\ -d & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$G_{2} = \begin{bmatrix} R_{2} & 0 \\ \hat{P}_{2}R_{2} & R_{2} \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 0 & -1 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$G = \begin{bmatrix} G_1 & G_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & -1 \\ 1 & 0 & 0 & 0 & 1 & 0 \\ -d & 0 & 0 & 0 & d & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & d & 0 & -d & 0 & 0 \end{bmatrix}$$